

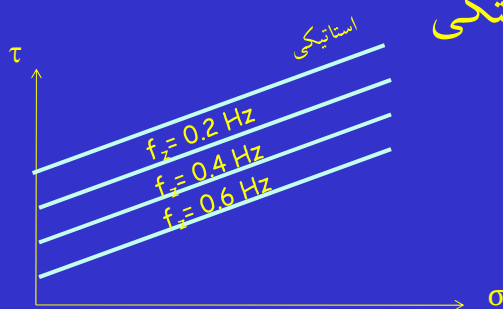
رفتار دینامیکی خاک ها

Hasan Ghasemzadeh

Soil dynamics

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پوش گسیختگی

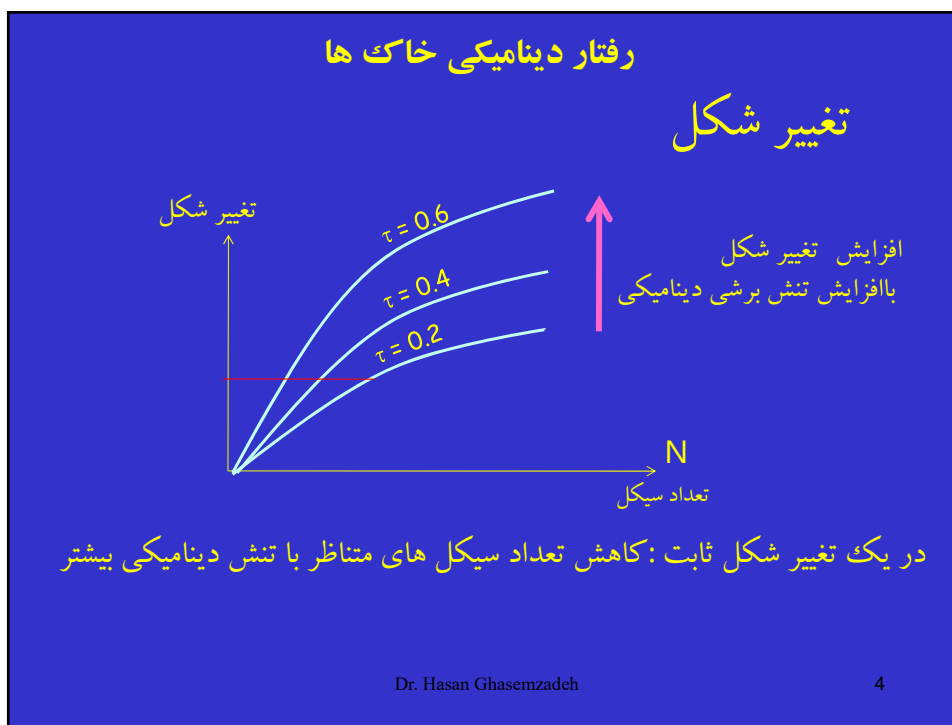
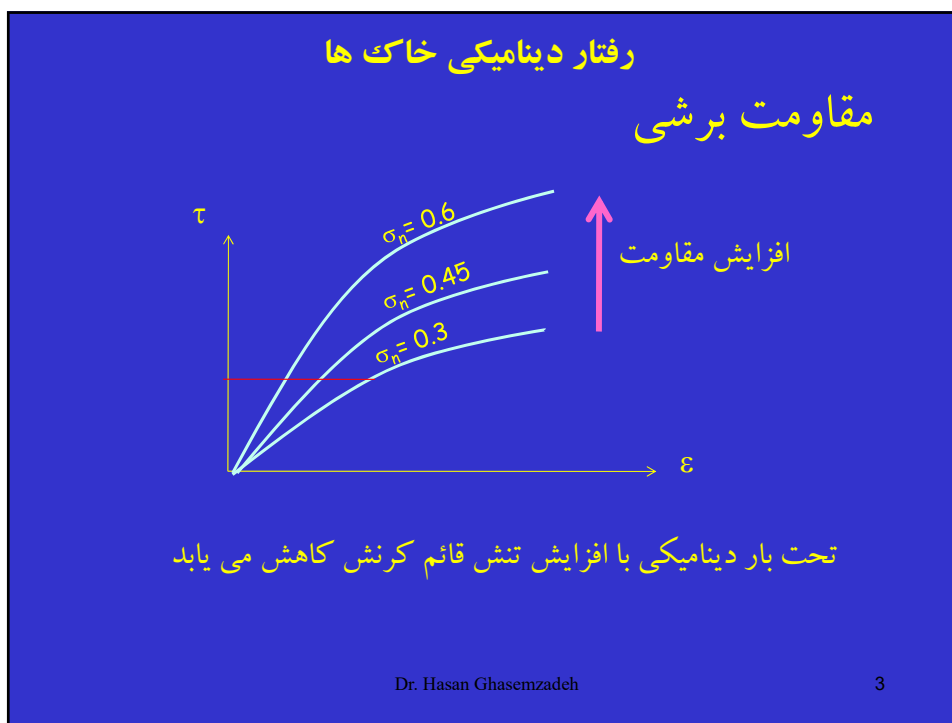


تحت بار دینامیکی

حرکت پوش به سمت پایین
کاهش چسبندگی
زاویه اصطکاک ثابت

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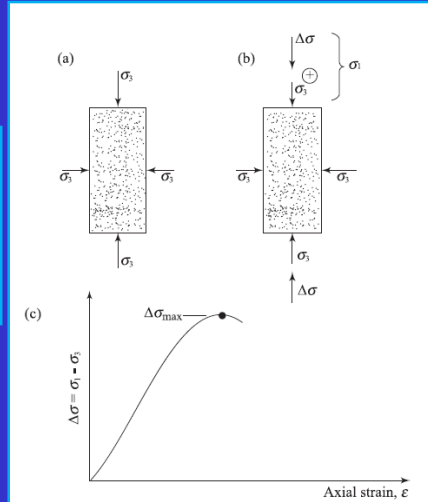
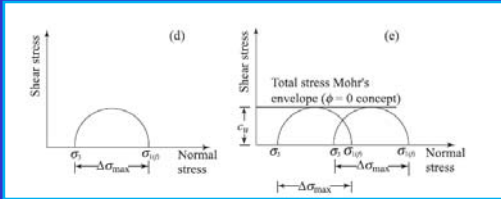
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مقدار تنش برشی زهکشی نشده

$$c_u = \frac{\Delta\sigma_{max}}{2} = \frac{\sigma_{1(f)} - \sigma_3}{2}$$

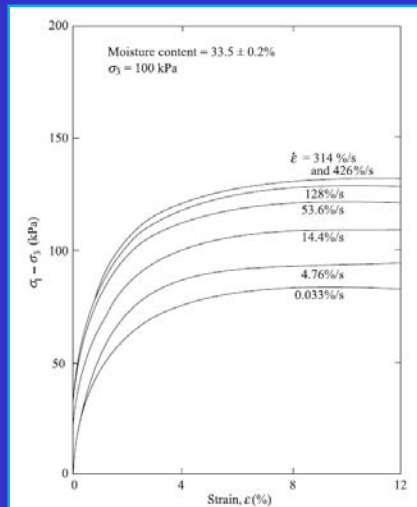


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$$\frac{c_{u(dynamic)}}{c_{u(static)}} \approx 1.5$$

Carroll suggestion (1963)



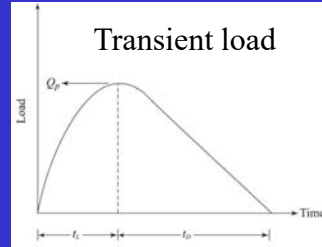
Unconsolidated-undrained triaxial test results on Buckshot clay

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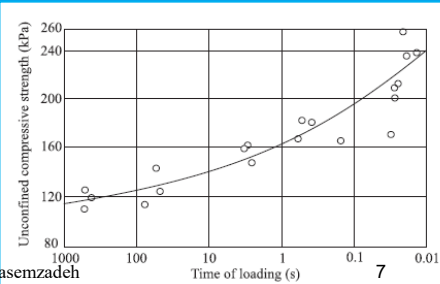
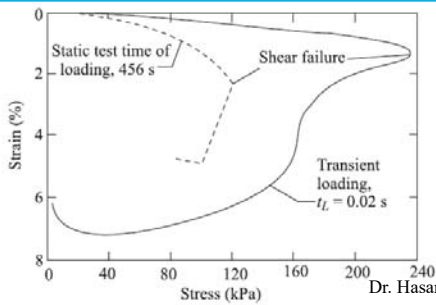
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$$\frac{q_u(\text{transient})}{q_u(\text{static})} \approx 1.5 \text{ to } 2$$

Casagrande and Shannon, 1949



Unconfined compressive strength of Cambridge clay

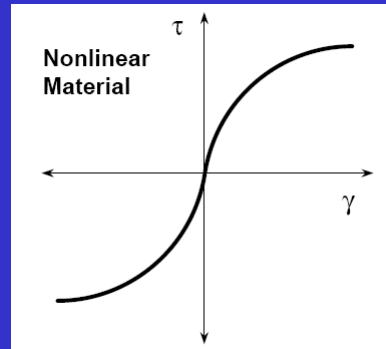
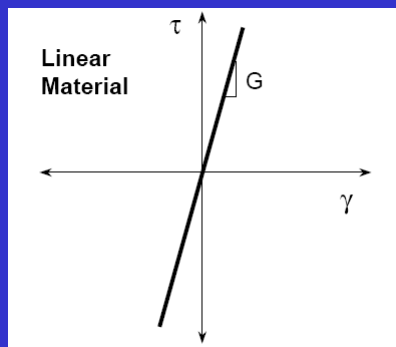


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Shear Modulus G

Defined as ratio of shear stress to shear strain



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Measurement of G_{max}

Usually accomplished by measuring V_s

Direct field measurement

- Seismic reflection
- Seismic refraction
- Seismic cross-hole
- Seismic downhole, uphole

Indirect field measurement

- Correlation to $(N_1)_{60}$, q_{c1} , etc.

Laboratory measurement

- Resonant column
- Bender element

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Shear Modulus G

Nonlinear Material

Secant Shear Modulus

$G_{sec} = \tau / \gamma$

Equivalent linear analysis

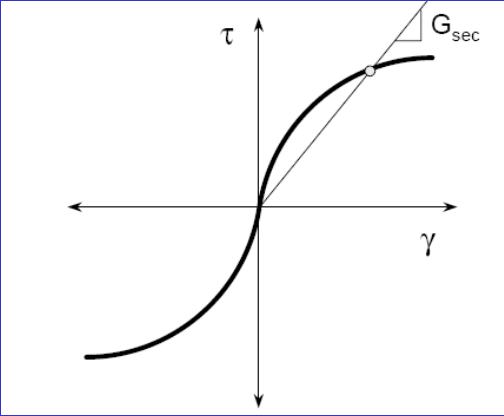
Tangent Shear Modulus

$G_{tan} = d\tau / d\gamma$

Nonlinear analysis

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رفتار دینامیکی خاک ها
Shear Modulus G_{sec}



Secant shear modulus, G_{sec} , decreases as shear strain increases

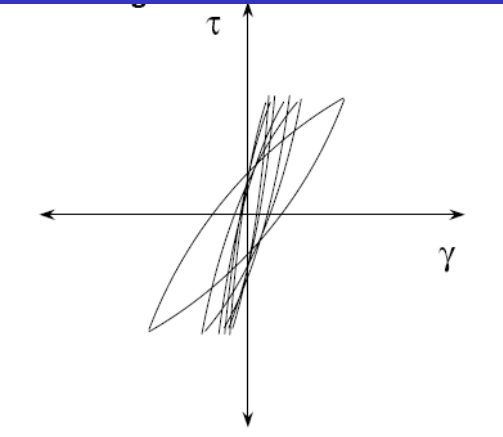
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Detailed description: The graph shows a non-linear relationship between shear stress τ and shear strain γ . The curve passes through the origin and exhibits strain softening. A secant line is drawn from the origin to a point on the curve, and its slope is labeled as G_{sec} .

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Shear Modulus G_{sec}

Cyclic loading

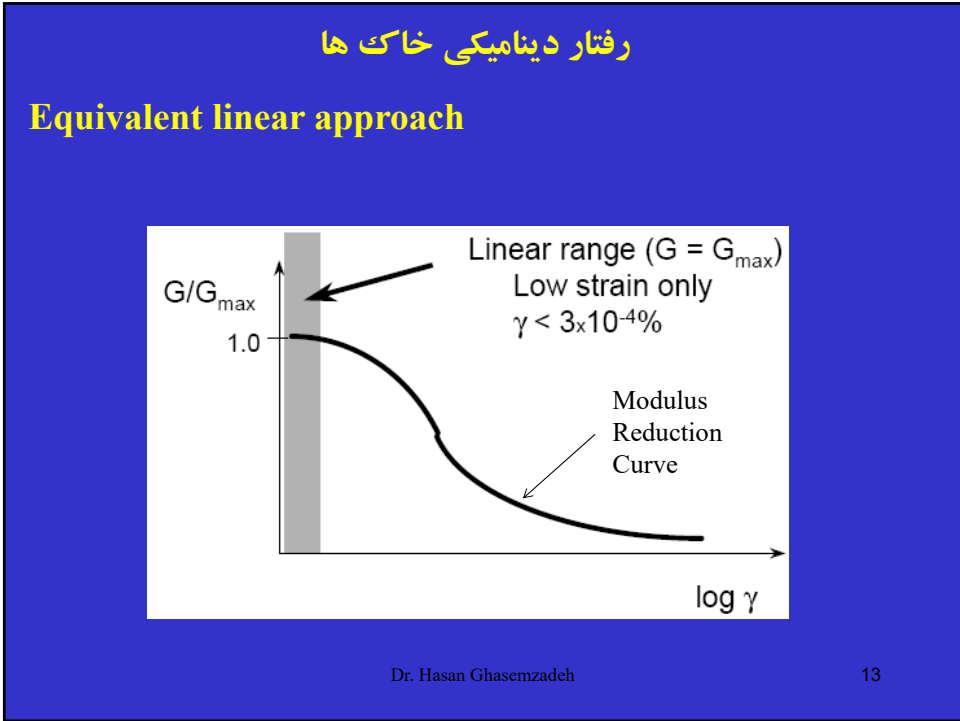


Secant shear modulus, G_{sec} , decreases as number of cycles increases

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Detailed description: The graph shows multiple hysteresis loops in the τ - γ plane, representing cyclic loading. The loops are nested, with the outermost loop having the largest area and the innermost having the smallest, indicating that the secant shear modulus decreases as the number of cycles increases.



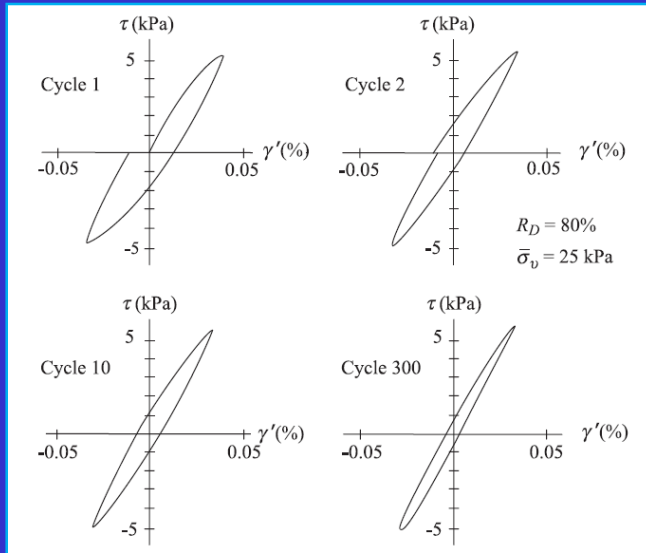
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Shear Modulus G_{max} Behavior

Increasing factor	G_{max}
Effective stress	Increases
Void ratio	Decreases
Geologic age	Increases
Cementation	Increases
Overconsolidation	Increases
Plasticity index	Negligible to small increase
Number of loading Cycles	Decreases for clay Increases for sand
Angle of friction	
Grain size characteristics	
Degree of saturation	
Level of strain	

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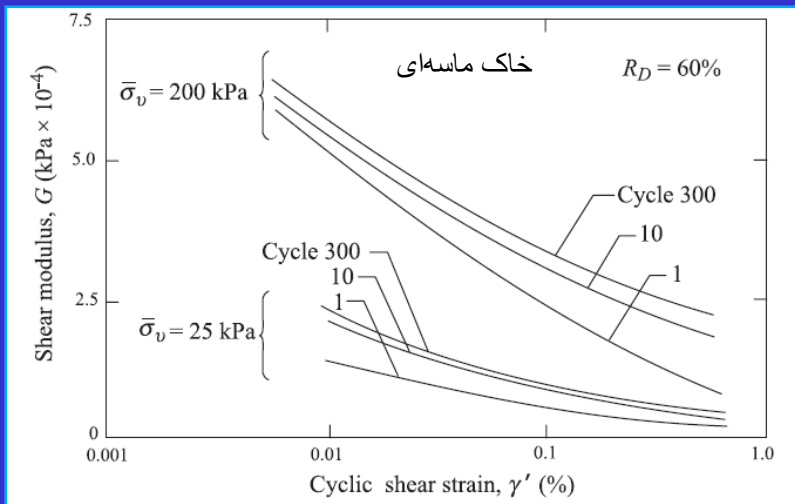


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منحنی تنش - کرنش ماسه متراکم

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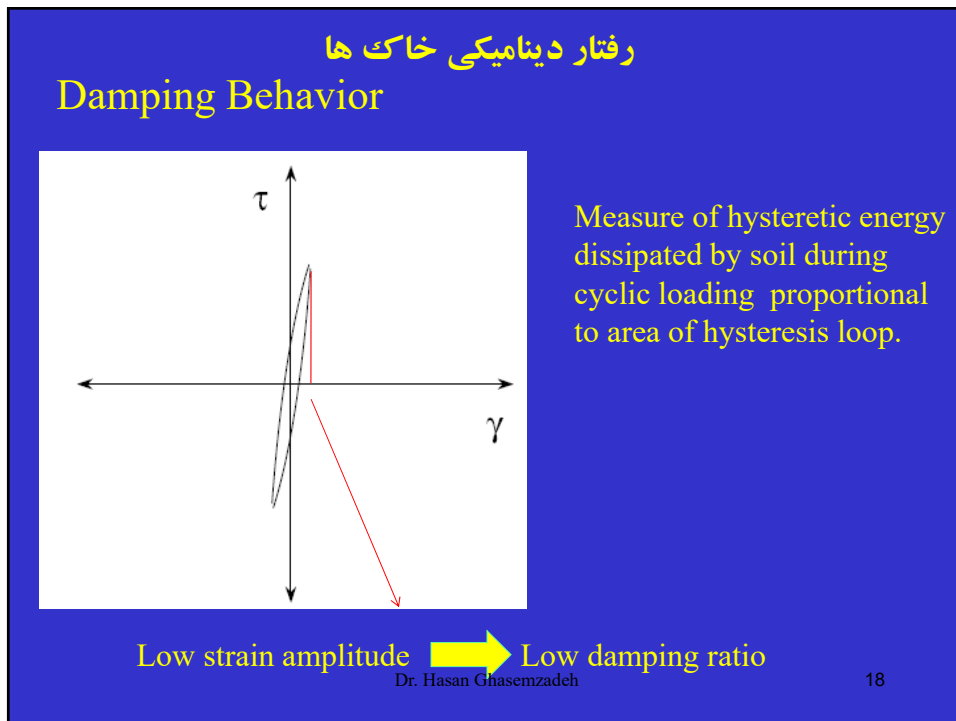
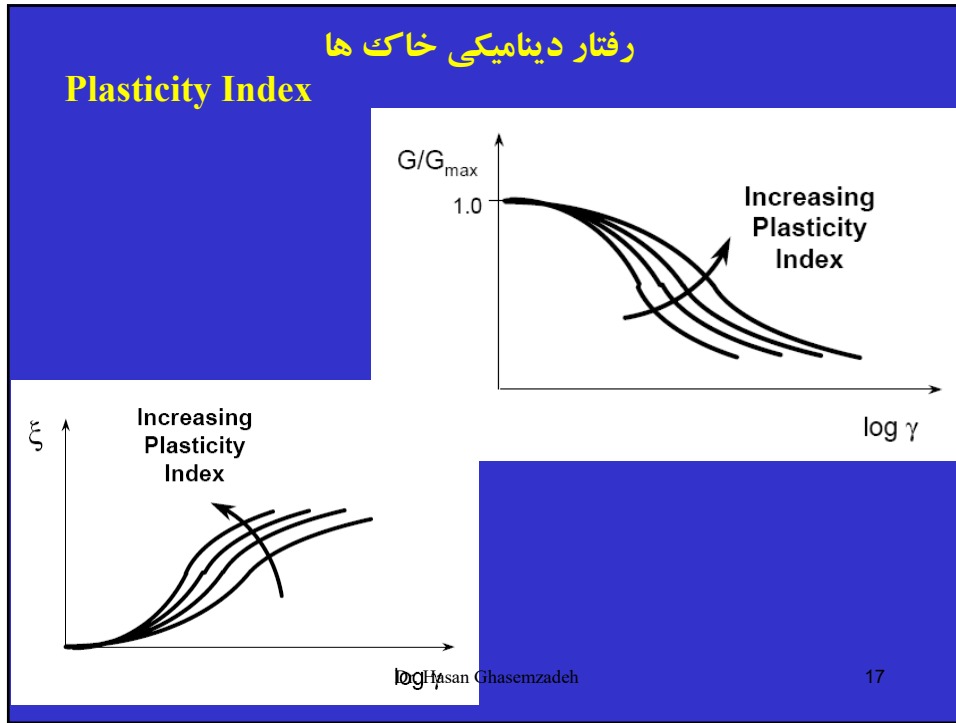
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تاثیر حلقه های بار گذاری بر مدول برشی



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Damping Behavior

$$\zeta = \frac{1}{2\pi} \frac{\Delta W}{W}$$

$$\zeta = \frac{\text{مساحت حلقه (لوپ)}}{2\pi(S_{OAB} + S_{OA'B'})}$$

High strain amplitude ➔ High damping ratio

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رفتار دینامیکی خاک ها

تاثیر حلقه های بارگذاری بر میرایی

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Experimental values of G_0

برای ماسه بازسازی در آزمایشگاه

Iwasaki & Tatsuoka

$$G_0 = AB \frac{(2.17 - e)^2}{1 + e} (\sigma'_0)^m$$

$14300 < A < 16000$ برای ماسه تمیز

$G_{\max} = 6908 \frac{(2.17 - e)^2}{1 + e} \sqrt{\bar{\sigma}_0}$

دانه های گرد گوشه

$G_{\max} = 3230 \frac{(2.97 - e)^2}{1 + e} \sqrt{\bar{\sigma}_0}$

دانه های گوشه تیز

$\bar{\sigma}_0 = \frac{\bar{\sigma}_v}{3} (3 - 2 \sin \phi)$

تنش قائم موثر

$\bar{\sigma}_v$

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Experimental values of G_0

$G = 218.82 K_2 \sqrt{\bar{\sigma}_0}$

$(\gamma' \leq 10^{-4} \%)$

برای دامنه های کرنش های کوچک

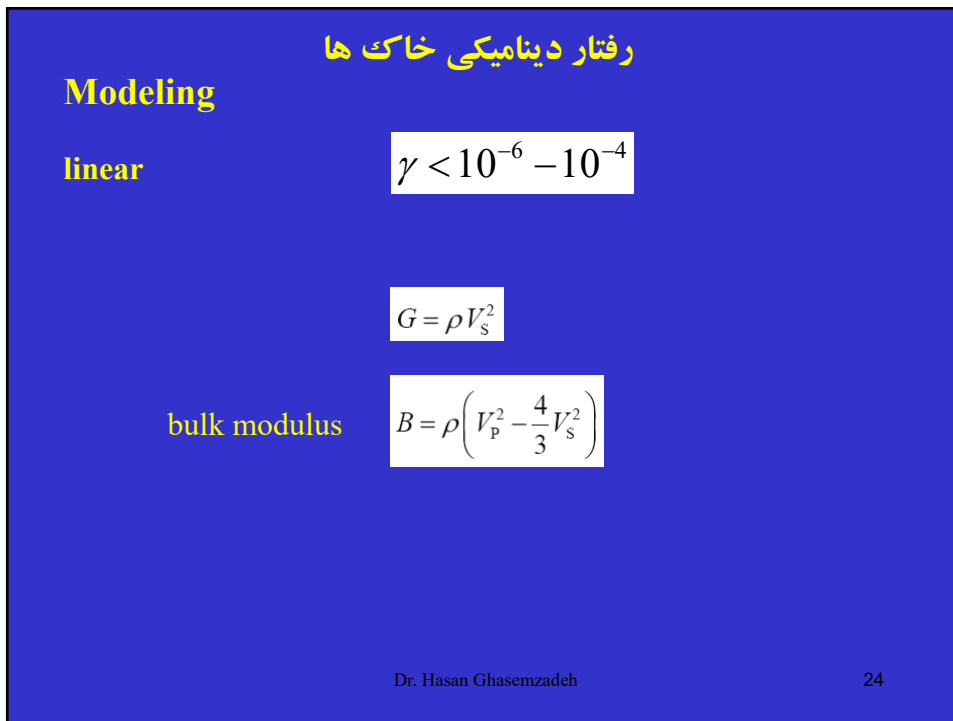
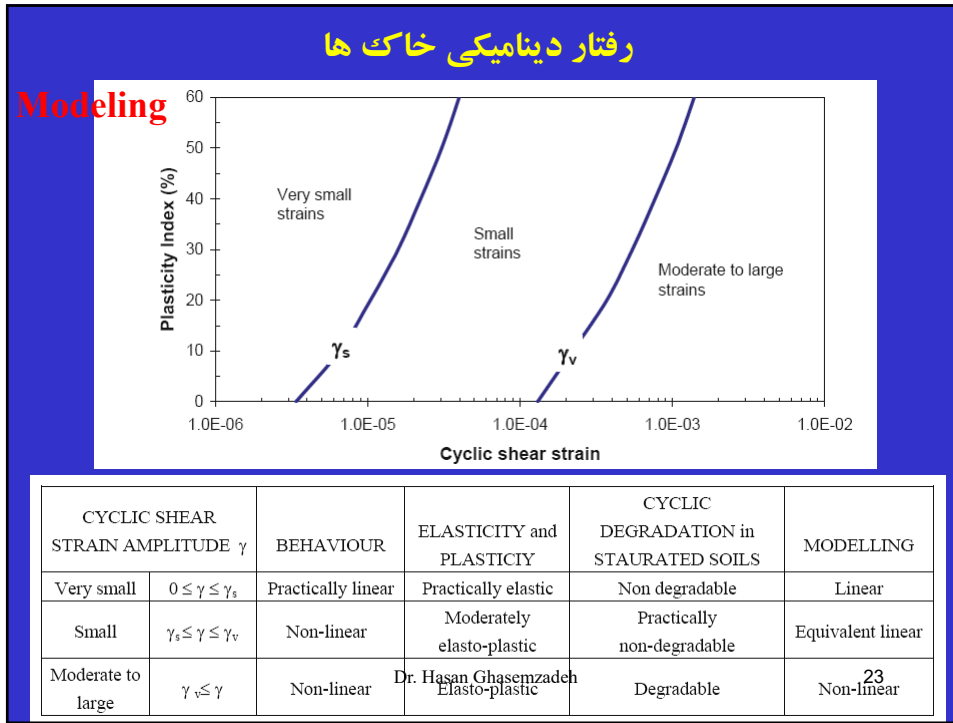
$G_{\max} = 218.82 K_{2(\max)} \sqrt{\bar{\sigma}_0}$

$\frac{G}{G_{\max}} = \frac{K_2}{K_{2(\max)}} F'$

Relative density,	
R_D (%)	$K_{2(\max)}$
30	34
40	40
45	43
60	52
75	61
90	70

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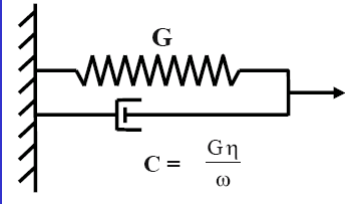


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Modeling

$$\gamma_s < \gamma < \gamma_v$$

Viscoelastic model



the viscoelastic model lends itself to an energy dissipation mechanism that is frequency dependent, in contradiction with experimental observation

$$\tau = G\gamma + C\dot{\gamma}$$

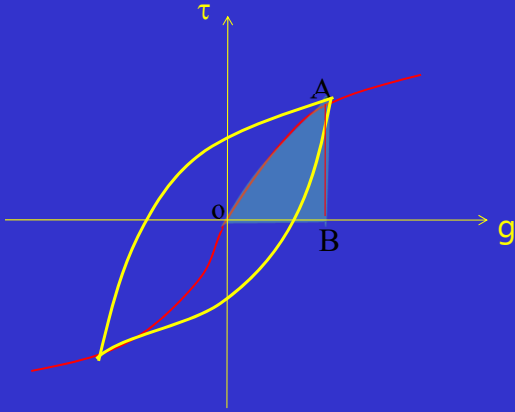
The normalizing quantity is the elastic energy W stored during one cycle Dr. Hasan Ghasemzadeh

$$W = \frac{1}{2} G \gamma_m^2$$

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Equivalent linear

$$< 10^{-2}$$


$$\zeta = \frac{1}{2\pi} \frac{\Delta W}{W}$$

$$\zeta = \frac{\text{مساحت حلقه (لوپ)}}{4\pi(S_{OAB})}$$

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Equivalent linear $\gamma_s < \gamma < \gamma_v$

$\gamma < 10^{-2}$

Equivalent linear **Bilinear**

Dr. Hasan Ghasemzadeh با افزایش تکرار کاهش می یابند

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Equivalent linear viscoelastic models

$\tau_m = G^* \gamma_m$

	COMPLEX MODULUS $G^* = \tau/\gamma$	DISSIPATED ENERGY IN ONE CYCLE ΔW	MODULUS $ G^* $
MATERIAL		$\pi G \eta \gamma_m^2$	G
MODEL 1	$G = [1 + i\eta]$	$\pi G \eta \gamma_m^2$	$G\sqrt{1 + \eta^2}$
MODEL 2	$G e^{i\theta}$ $\eta = 2 \sin(\theta/2)$	$\pi G \eta \gamma_m^2 \sqrt{1 - \frac{\eta^2}{4}}$	G
MODEL 3	$G [\sqrt{1 - \eta^2} + i\eta]$	$\pi G \eta \gamma_m^2$	G

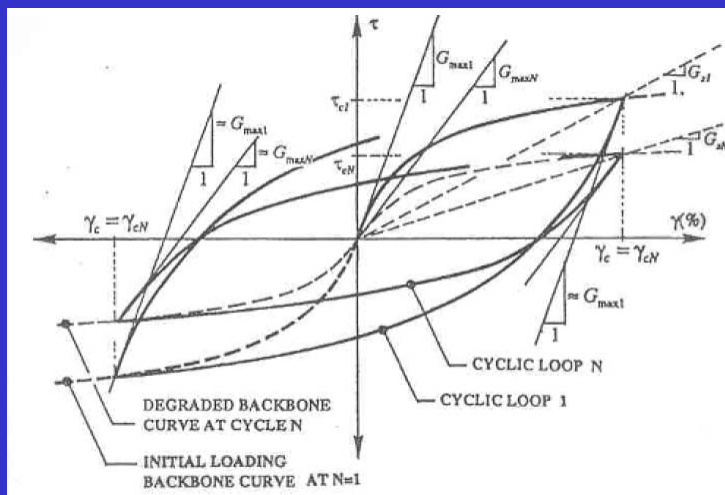
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Modeling
Nonlinear

$\gamma_v \leq \gamma$

$\gamma > 10^{-2}$



Stiffness degradation with the number of cycles

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